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TITLE: Composite Material, Method for the Production of  
a Composite Material and the Utilization Thereof

TRANSLATOR'S DECLARATION

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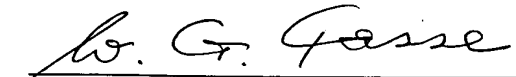
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**PCT International Application PCT/DE2004/002175,  
as filed on September 30, 2004**

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ACCURATE LITERAL TRANSLATION OF PCT INTERNATIONAL APPLICATION  
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Composite Material, Method for the Production of a Composite  
Material and the Utilization Thereof

The invention relates to a composite material, a method for  
producing composite material and to the use thereof.

5 Modern gas turbines particularly aircraft engines must satisfy  
the highest demands regarding reliability, weight, power output,  
efficiency and their life duration. During the last decades  
aircraft engines have been developed particularly in the civil  
sector, which engines fully satisfy the above demands. These  
10 aircraft engines have reached a high degree of technical  
perfection. In the design of aircraft engines the selection of  
the materials plays, among other things, a critical role. This  
applies also to the search for new suitable materials.

The most important materials that are used these days for  
15 aircraft engines or other gas turbines are titanium alloys,  
nickel alloys, also referred to as super alloys, and high  
strength steels. The high strength steels are used particularly  
for shaft components, gear components, and for compressor  
housings and turbine housings. Titanium alloys are typical  
20 alloys for compressor components while nickel alloys are  
suitable for the hot components of the aircraft engine.

A very promising group of a new material for future generations of aircraft engines are so-called fiber reinforced composite materials. Modern composite materials comprise a matrix material which may be made of a polymer, a metal, or ceramic matrix and fibers embedded into the matrix material.

The present invention relates to a composite material in which the matrix is made as a metal matrix. Such a material is referred to as a metal matrix composite material, in short MMC. In connection with high strength MMC materials in which titanium is used as matrix material, the weight of the structural components can be reduced up to 50% compared to conventional titanium alloys. Fibers of high strength and a high modulus of elasticity are used as reinforcements.

Such fiber reinforced composite materials are known in the prior art. Thus, European Patent Publication EP 0 490 629 B1 discloses a pre-shaped blank for a composite material including a foil whereby the foil comprises a groove and a thread shaped reinforcement arranged in the groove, and wherein the pre-shaped blank has the shape of a ring or of a disc. For the production of a multi-ply composite structure one proceeds according to European Patent Publication EP 0 490 629 B1 in such a way that several such pre-shaped blanks are stacked whereby the pre-shaped blanks are consolidated under the influence of heat and pressure to form a fully dense composite material. Further composite materials and methods for their production are known from

European Patent Publication EP 0 909 826 B1, from US Patent 4,697,324 and from US Patent 4,900,599.

Starting with the above prior art the problem underlying the invention is to provide a new composite material and a new method  
5 for producing composite materials.

This problem is being solved by a composite material with the characteristics defined in patent claim 1. The composite material comprises a matrix material and at least one fiber embedded in the matrix material. According to the invention a  
10 composite of matrix material and fibers is present within an inner section, whereas the matrix material is present exclusively in an outer section, and wherein the fibers reach to different extents into the outer section, in which the matrix material is exclusively present, for a strength optimizing intermeshing of  
15 the inner section with the outer section.

According to an advantageous further embodiment of the invention, the fibers neighboring an inwardly positioned opening terminate with an equal spacing from the opening, whereas next to the outer section in which the matrix material is exclusively present, the  
20 spacing is formed to vary.

The method according to the invention for producing a composite material is defined in the independent claim 6. The method serves for the production of a composite material of a matrix

material and of at least one fiber embedded into the matrix material.

Preferably a recess (or groove) is formed in the disc whereby the groove has a depth larger than the diameter of the fiber in such a way that lands of the matrix material project above the fiber inserted into the groove.

According to an advantageous further development of the method according to the invention the fiber or each fiber is inserted into the groove or into each groove of the respective disc in such a way that a composite of matrix material and fiber is present in an inner section whereas in an outer section the matrix material is exclusively present. The discs are stacked in such a way that the fibers of the stacked discs reach to varying extents into an outer section in which the matrix material is exclusively present for a strength optimizing intermeshing between the inner section and the outer section.

Preferred further embodiments of the invention are defined by the dependent claims and the following description.

Example embodiments of the invention are described in more detail with reference to the drawing without being limited thereto. The drawings show:

Fig. 1 a schematic cross section of a disc of matrix material;

- Fig. 2 a substantially magnified cutout of the disc of Figure 1 with a recess (or groove) formed in the disc;
- Fig. 3 the arrangement according to Figure 1 with a fiber inserted into the groove;
- 5 Fig. 4 a schematic cross section of a disc of matrix material with an embedded fiber;
- Fig. 5 the detail V of Figure 4;
- Fig. 6 a schematic cross section of a plurality of matrix material discs with embedded fibers stacked one on top of the other;
- 10 Fig. 7 a cutout of the arrangement of Figure 6; and
- Fig. 8 a schematic cross section of a composite material according to the invention.

Referring to Figures 1 to 8 details of the composite material according to the invention and details of the method according to the invention for producing the composite material will now be described in more detail.

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The composite material according to the invention comprises a matrix material of titanium or of a titanium alloy as well as several fibers embedded in the matrix material. The fibers are preferably ceramic fibers made of silicon carbide (SiC). The composite material according to the invention is formed of several discs of matrix material whereby a fiber is embedded in each disc. A plurality of such discs with a fiber embedded therein are stacked one on top of the other and interconnected with each other to form the composite material according to the

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invention. A groove is formed in the respective disc of matrix material for the embedding of the fiber. The respective fiber is inserted into the groove and surrounded by matrix material on all sides so that the fiber is embedded in the disc.

5 Fig. 1 shows, in a substantially schematic cross section, a disc of matrix material, namely titanium. A bore 11 (or hole) is provided in a central section of the disc 10.

10 According to a first step of the method of the invention for producing the composite material according to the invention, a recess (or groove) is formed in a facing side 12 of the disc 10. Fig. 2 shows a substantially magnified detail of the disc 10 in the area of the facing side 12. The recess 13 which is formed in the facing side 12 of the disc 10 is a spiral groove. The spiral groove accordingly extends exclusively on a facing side  
15 12 of the disc 10 from the inside of the disc 10 outwardly.

A fiber 14 is inserted into the spiral groove 13 after the formation of the spiral groove 13 in the top side 12 of the disc 10. It can be seen from Fig. 3, that lands 15 of matrix material  
20 project above the inserted fiber 14. Thus, the depth of the spiral groove 13 is larger than the diameter of the fiber 14.

Due to the groove 13 an exact guiding of the fiber 14 is assured. The position of the fiber 14 within the disc 10, namely within the matrix material, is thus exactly predetermined.

According to a further step of the method of the invention, the arrangement of Fig. 3 is subjected to a super-plastic deformation process. For this purpose the disc 10 or rather the matrix material is heated to a deformation temperature and subjected to a uniaxially directed pressure so that the lands 15 are deformed in a super-plastic manner in such a way that subsequently the fiber 14 is completely surrounded by the matrix material as shown in Fig. 5 so that the fiber 14 is embedded in the matrix material. Fig. 5 shows that the position of the fiber 14 is maintained even after the super-plastic deformation of the lands 15. The super-plastic deformation densifies the matrix material.

Fig. 4 shows a substantially schematic cross section of the disc 10 of matrix material with the fiber 14 embedded in the disc 10. The fiber 14 is surrounded on all sides by the matrix material and thus embedded in the matrix material.

Referring to Fig. 6, in the next step of the inventive method for producing the actual composite material, a plurality of discs 10 with fibers 14 embedded in the discs 10 are arranged one on top of the other so that in this manner a ring-shaped or cylinder-shaped stack is formed. The discs 10 arranged one above the other and stacked are then joined or interconnected with each other by diffusion welding under a small axial pressure. Thus, the composite material according to the invention is completed.



Prior to stacking the discs 10 as shown in Fig. 6 it is preferred to inspect (or check) the discs 10 with the fibers 14 embedded therein for cracks in the matrix material and for breaks in the fibers 14. This inspection can be performed by ultrasound, x-rays, or tomography. If a crack or a break is ascertained, the disc 10 is discarded. When the inspection shows that no crack and no break in the fiber 14 is present, the disc 10 can be used for the stacking.

Fig. 7 shows a cutout of the arrangement according to Fig. 6 in an area of three stacked discs 10 which are joined to each other. Thus Fig. 7 shows that the fiber 14 embedded in one disc 10 is staggered relative to the fibers 14 in the two neighboring discs 10. This staggering provides a hexagonal packing of the fibers 14. As shown in Fig. 7, the fiber 14 extends in a spiral in such a way within the disc 10 that in the cross section the resulting centers of the fibers of one disc 10 are arranged between the respective centers of the fiber 14 in a neighboring disc 10.

Fig. 6 shows that each fiber 14 in each disc 10 ends with a spacing from an outer, lateral end (or edge) of the respective disc. According to Fig. 6 this spacing varies or differs for each disc. On the other hand, next to the opening 11 positioned inwardly, the lateral spacing of the fibers 14 from the opening 11 is equal (for all fibers). With the aid of the varying or different lateral spacings between the fibers 14 and the outer lateral end (or edge) of the disc 10 it is possible to achieve gradual variations in the elastic characteristics of the

composite material. Furthermore an intermeshing is achieved between the non-reinforced sections and the fiber reinforced sections of the composite material whereby the strength characteristics thereof are positively influenced.

5 Fig. 8 shows a substantially schematic cross section through a composite material according to the invention which was produced as described above. According to Fig. 8 fibers 14 are embedded in the matrix material in an inwardly positioned section 16 of the composite material. The matrix material however is  
10 exclusively present in an outwardly positioned section 17. This means that in the outwardly positioned section 17 only titanium is present. This feature has an advantage when the composite material must be further machined for example by milling, because the fibers 14 must not be damaged by the milling. A subsequent  
15 milling operation of the composite material is thus considered exclusively in the area of the section 17 in which the matrix material is exclusively present. Further, Fig. 8 shows again that next to the inwardly positioned opening the fibers 14 end with an equal spacing to the opening whereas at the outer end (or  
20 edge) next to the section 17, in which the matrix material is present exclusively, this spacing is formed to vary. The radial stepping of the fibers 14 in the section 16 relative to the section 17 has the effect of providing a strength optimizing intermeshing of the two sections 16 and 17.

Following the above described method according to the invention for producing the composite material according to the invention the procedure is roughly summarized as follows.

In a first step several discs of matrix material, namely titanium, are provided on their facing side with a spiral recess or groove. In a second step a fiber of silicon carbide is inserted into this spiral groove. Thereafter, in a third step the disc, with the fiber inserted into the disc, is consolidated by a super-plastic deformation. As a result, the fiber is surrounded on all sides by matrix material or embedded into the matrix material. In a next step the so produced discs with the fibers embedded in the discs are tested for cracks in the matrix material and for breaks in the fibers. If this testing shows that there is no crack nor any fiber break, the respective discs are stacked to form rings. The stack of a plurality of discs is then subjected, in a further step of the method according to the invention, to a diffusion welding so that neighboring discs are interconnected with each other. Upon completion of this joining step the composite material may in a further step be subjected to a finishing machining, for example by milling.

The method according to the invention is reliable and cost efficient. The method according to the invention can be performed in a fully automated process with an integrated testing thereby assuring quality. Since each disc is tested with regard to its quality, faults or defects in the composite material can be timely discovered and thus avoided. Such testing reduces

rejects. A further advantage is seen in that the exact position of the fibers in the composite material is predetermined and maintained. The spiral arrangement of the fibers in the composite material is preferred. However other more complex fiber guiding is also possible, for example a star shaped fiber guiding. According to the invention a titanium coating of the fibers as is required in the prior art, is not necessary. A further advantage resides in that no extremely long fibers need to be used. Due to the guiding of the fibers in the grooves it is possible to use fibers of finite length.

The composite material according to the invention distinguishes itself, thus, by an exact position of the fibers within the matrix material. The composite material according to the invention is formed by a plurality of joined discs of matrix material whereby a spirally extending fiber is embedded in each disc. The fibers end with a spacing from a lateral outer end (edge) of the composite material so that in an outer section thereof the matrix material is exclusively present, whereby in this section a later milling operation can be performed on the composite material. For completeness sake it should be mentioned that several fibers may be embedded in one groove and that several grooves which are nested one within the other may be formed in one disc. Here again each of these grooves may hold one or several fibers. However, the shown example embodiment in which each disc has one groove for receiving one fiber, is preferred.

The composite material according to the invention is particularly suitable for use as a material for producing rings with integral blades for aircraft engines, which are also referred to as so-called bladed rings (blings).